

26 **1. Introduction**

27 A potable water supply system can be divided into four main works: raw water
28 collection work, purification work, transmission work, and distribution work. Among
29 these works, a water distribution network (WDN) plays a critical role in conveying
30 potable water from its sources to various end-users, serving residential, commercial,
31 industrial and firefighting purposes. Typically, a WDN constitutes the largest portion in
32 terms of size and pipe length and is the most complex system to manage. In a WDN, three
33 primary types of losses can occur: water loss, energy loss, and water quality deterioration.
34 To control and mitigate these losses, the audit method that classifies each component in
35 the balance has proven to be an effective tool for identifying the components responsible
36 for the losses, calculating the performance, and benchmarking against other water
37 utilities.

38 The water audit method was introduced by the International Water Association
39 (IWA) to classify all water volume inputs, outputs, and losses in a WDN in the
40 accountable water balance (Alegre et al. 2006). The IWA water balance is globally
41 recognized as the best practice for assessing water losses and has been adopted and
42 extended by the American Water Works Association (AWWA 2016). The water balance
43 approach allows for the calculation of performance indicators, which are used for
44 benchmarking, performance comparison, and setting performance targets (Wu et al.
45 2011).

46 Similar to the concept of water balance, the energy balance focuses on energy
47 inputs, outputs, and losses in a WDN. The International Energy Agency (IEA, 2016)
48 estimated that the water sector consumed 4% of the world's total electricity in 2014, with
49 projections indicating an 80% increase by 2040. According to the World Bank (2012),

50 electricity costs account for 5% to 30% of the total operating expenses for water and
51 wastewater utilities worldwide. Cabrera et al. (2010) introduced the concept of an energy
52 audit in WDNs, focusing on energy consumption components, especially those associated
53 with leakages. Mamade et al. (2015) added new components of energy consumption such
54 as valves, pumps, and turbines into the energy balance. Several real-world case studies
55 have evaluated energy losses due to leakage (Dziedzic and Karney 2015; Lapprasert et
56 al. 2018; Lenzi et al. 2013; Lipiwattanakarn et al. 2019; Lipiwattanakarn et al. 2021a).
57 Additionally, Pardo et al. (2019) developed a MATLAB-based energy balance software
58 capable of evaluating energy losses due to friction and leakage.

59 Chlorine loss presents a critical concern for water quality in WDNs. The World
60 Health Organization (WHO, 2011) has established a minimum free residual chlorine
61 requirement of 0.2 mg/l for ensuring the safe use of potable water. A pioneering concept
62 of the chlorine mass balance was introduced by Lipiwattanakarn et al. (2021b) to assess
63 chlorine losses in WDNs. The chlorine mass input is divided into three components: mass
64 delivered to users, outgoing mass through water losses, and mass losses due to chemical
65 reactions, following the same concepts of water and energy balances. In a recent study,
66 Wongpeerak et al. (2023) introduced straightforward equations for assessing chlorine
67 mass losses based on a simple theoretical analysis.

68 EPANET software (Rossman, 2000) is renowned for its simulation capabilities in
69 WDNs. However, it currently lacks the functionality to assess water, energy, and chlorine
70 mass balances. Manually analyzing these three balances in complex WDNs can be
71 troublesome and prone to errors due to the system's intricacy. Therefore, we have
72 developed the first software, KU2EPA-Balances, capable of conducting comprehensive
73 analyses of all three balances. This software, built on the Python programming language,

74 utilizes the Water Network Tool for Resilience (WNTR) (Klise et al., 2017), compatible
 75 to EPANET, to provide precise results to users.

76 **2. Balance Calculations**

77 The calculations can be divided into three sections, corresponding to the three
 78 types of balances as follows.

- 79 • Water balance calculation

80 Figure 1 shows the water balance components for WDNs in this study. On the
 81 input side, the system input volume (W_{IN}) represents the total water volume entering a
 82 WDNs and can come from reservoirs ($W_{IN,RES}$), tanks ($W_{IN,TANK}$), and junctions
 83 ($W_{IN,JUNC}$). The output side comprises of two primary components: water outgoing
 84 through nodes (W_{OUT}) and water loss (W_{LOSS}). W_{OUT} can be further categorized into water
 85 delivered to users ($W_{OUT,USER}$), water outgoing to reservoirs ($W_{OUT,RES}$), and water
 86 outgoing to tanks ($W_{OUT,TANK}$). In this study, W_{LOSS} represents the cumulative leakage
 87 flow, which is pressure-dependent.

System input volume W_{IN}	Input water from reservoirs $W_{IN,RES}$	Water outgoing through nodes W_{OUT}	Water delivered to users $W_{OUT,USER}$
	Input water from tanks $W_{IN,TANK}$		Water outgoing to reservoirs $W_{OUT,RES}$
	Input water from junctions $W_{IN,JUNC}$		Water outgoing to tanks $W_{OUT,TANK}$
	Water loss W_{WL}		

88 **Figure 1. Water balance components**

89 For a defined period, each component can be calculated using the results from
 90 the network simulation model, as follows:

$$W_{IN,TYPE} = \sum_{i_t=1}^{n_t} \sum_{i_{I,TYPE}=1}^{n_{I,TYPE}} Q_{i_{I,TYPE},i_t}(t)\Delta t \quad (1)$$

$$W_{OUT,TYPE} = \sum_{i_t=1}^{n_t} \sum_{i_{O,TYPE}=1}^{n_{O,TYPE}} Q_{i_{O,TYPE},i_t}(t)\Delta t \quad (2)$$

$$W_{WL} = \sum_{i_t=1}^{n_t} \sum_{i_{WL}=1}^{n_{WL}} q_{i_{WL},i_t}(t)\Delta t \quad (3)$$

$$q_{WL,i_t} = c_{i_{WL},i_t} \cdot P_{i_{WL},i_t}^{N_1} \quad (4)$$

91

92 where Q represents the discharge at a node, t denotes time, and Δt stands for the time
 93 interval. i and n are defined as an index and the total count of an index, respectively. The
 94 subscripts of i and n are t , I , O , $TYPE$, and WL , denoting time, input, output, type of
 95 node, and water loss, respectively. Thus, $TYPE$ can be RES , $TANK$, and $JUNC$, defined
 96 as reservoirs, tanks, and junctions, respectively. Furthermore, q is the leak discharge at
 97 each junction calculated by the emitter function relating with pressure (P), while c and N_1
 98 are the emitter coefficient and exponent, respectively.

99 • Energy balance calculation

100 The energy balance components, as illustrated in Figure 2, provide details about
 101 the input, output, and loss side of energy in a WDN. On the input side, the system input
 102 energy (E_{IN}) represents the total energy entering a WDN and can come from reservoirs
 103 ($E_{IN,RES}$), tanks ($E_{IN,TANK}$), and junctions ($E_{IN,JUNC}$). The output side comprises two
 104 primary components: energy outgoing through nodes (E_{OUT}) and energy outgoing through
 105 water loss (E_{WL}). On the loss side, the term the energy dissipated (E_{LOSS}) represents the
 106 cumulative energy losses in a WDN, stemming from friction in pipes ($E_{LOSS,PIPE}$) and
 107 valves ($E_{LOSS,VALVE}$).

System input energy E_{IN}	Input energy by reservoirs $E_{IN,RES}$	Energy outgoing through nodes E_{OUT}	Energy delivered to users $E_{OUT,USER}$
	Input energy by tanks $E_{IN,TANK}$		Energy outgoing to reservoirs $E_{OUT,RES}$
			Energy outgoing to tanks $E_{OUT,TANK}$
	Input energy by junctions $E_{IN,JUNC}$	Energy dissipated E_{LOSS}	Energy loss by pipe friction $E_{LOSS,PIPE}$
	Input energy by pumps $E_{IN,PUMP}$		Energy loss by valves $E_{LOSS,VALVE}$
		Energy outgoing through water loss E_{WL}	

108 **Figure 2. Energy balance components**

109 Each component for a defined period can be calculated by using the results from
110 the network model, which can be computed as follows:

- 111 - Input energy to the system by reservoirs, tanks, and junctions

$$E_{IN,TYPE} = \gamma \cdot \sum_{i_t=1}^{n_t} \sum_{i_{I,TYPE}=1}^{n_{I,TYPE}} Q_{i_{I,T},i_t}(t) * H_{i_{I,T},i_t}(t) \Delta t \quad (5)$$

112

- 113 - Input energy to the system by pumps

$$E_{IN,PUMP} = \gamma \cdot \sum_{i_t=1}^{n_t} \sum_{i_{I,PUMP}=1}^{n_{I,PUMP}} Q_{i_{I,PUMP},i_t}(t) * -\Delta H_{i_{I,PUMP},i_t}(t) \Delta t \quad (6)$$

114

- 115 - Energy outgoing through nodes

$$E_{OUT,TYPE} = \gamma \cdot \sum_{i_t=1}^{n_t} \sum_{i_{O,TYPE}=1}^{n_{O,TYPE}} Q_{i_{O,T},i_t}(t) * H_{i_{O,T},i_t}(t) \Delta t \quad (7)$$

116 - Energy outgoing through water loss

$$E_{WL} = \gamma \cdot \sum_{i_t=1}^{n_t} \sum_{i_{WL}=1}^{n_{WL}} q_{i_{WL},i_t}(t) * H_{i_{WL},i_t}(t) \Delta t \quad (8)$$

117

118 - Energy losses in the system by pipe friction and valves

$$E_{LOSS,PIPE} = \gamma \cdot \sum_{i_t=1}^{n_t} \sum_{i_{L,PIPE}=1}^{n_{L,PIPE}} Q_{i_{L,T},i_t}(t) * \Delta H_{i_{L,T},i_t}(t) \Delta t \quad (9)$$

$$E_{LOSS,VALVE} = \gamma \cdot \sum_{i_t=1}^{n_t} \sum_{i_{L,VALVE}=1}^{n_{L,VALVE}} Q_{i_{L,T},i_t}(t) * \Delta H_{i_{L,T},i_t}(t) \Delta t \quad (10)$$

119

120 where H represents the energy head at a node, ΔH denotes head loss, and γ stands for the
121 specific weight of water. The additional subscripts of i and n are L , $PIPE$, $VALVE$, and
122 $PUMP$, denoting loss, pipe, valve, and pump, respectively. In the EPANET model, pumps
123 are categorized as a link type, so pump head is considered as negative head loss.

124 • Chlorine mass balance calculation

125 Figure 3 illustrates the components of the chlorine mass balance in WDNs in this
126 study. It provides details about the input, output, loss, and changes sides. On the input
127 side, the system input mass (M_{IN}) represents the total chlorine mass entering a WDN. The
128 output side comprises two components: mass delivered to users (M_{USER}) and outgoing
129 mass through water losses (M_{WL}). On the loss side, the mass losses by reactions (M_{RT})
130 represent the total chlorine mass loss in a WDN, which can come from pipes ($M_{RT,PIPE}$)
131 and tanks ($M_{RT,TANK}$). On the changes side, the mass changes in networks (ΔM_N) represent

132 the total mass change in a WDN, which can come from pipes ($\Delta M_{N,PIPE}$) and tanks
 133 ($\Delta M_{N,TANK}$).

System input mass M_{IN}	Mass delivered to users M_{USER}	
	Outgoing mass through water losses M_{WL}	
	Mass losses by reactions M_{RT}	Mass losses by reactions in pipes $M_{RT,PIPE}$
		Mass losses by reactions in tanks $M_{RT,TANK}$
	Mass changes in networks ΔM_N	Mass changes in pipes $\Delta M_{N,PIPE}$
		Mass changes in tanks $\Delta M_{N,TANK}$

134 **Figure 3. Chlorine mass balance components**

135 For the input and output chlorine mass balance components, each component for
 136 a defined period can be calculated by the cumulative of the product between the chlorine
 137 concentration (C) and the discharge (Q) for a defined period (Δt) as follows:

138 - System input chlorine mass

$$M_{IN} = \sum_{i_t=1}^{n_t} \sum_{i_l=1}^{n_l} C_{i_l,i_t}(t) Q_{i_l,i_t}(t) \Delta t \quad (11)$$

139 - Mass delivered to users

$$M_{USER} = \sum_{i_t=1}^{n_t} \sum_{i_{USER}=1}^{n_{USER}} C_{i_{USER},i_t}(t) Q_{i_{USER},i_t}(t) \Delta t \quad (12)$$

140 - Outgoing mass through water losses

$$M_{WL} = \sum_{i_t=1}^{n_t} \sum_{i_{WL}=1}^{n_{WL}} C_{i_{WL},i_t}(t) Q_{i_{WL},i_t}(t) \Delta t \quad (13)$$

141 - Mass losses by reactions

$$M_{RT} = M_{RT,PIPE} + M_{RT,TANK} \quad (14)$$

$$M_{RT,PIPE} = \sum_{i_t=1}^{n_t} \sum_{i_{PIPE}=1}^{n_{PIPE}} R_{i_{PIPE},i_t}(t) \forall_{i_{PIPE},i_t}(t) \Delta t \quad (15)$$

$$M_{RT,TANK} = \sum_{i_t=1}^{n_t} \sum_{i_{TANK}=1}^{n_{TANK}} R_{i_{TANK},i_t}(t) \forall_{i_{TANK},i_t}(t) \Delta t \quad (16)$$

142 where R represents the decay rate of chlorine concentration by chemical reactions and \forall
 143 means the water volume in each pipe or tank.

144 - Mass changes in networks

$$\Delta M_N = \Delta M_{N,PIPE} + \Delta M_{N,TANK} \quad (17)$$

$$\Delta M_{N,PIPE} = M_{N,PIPE}(t_f) - M_{N,PIPE}(t_o) \quad (18)$$

$$\Delta M_{N,TANK} = M_{N,TANK}(t_f) - M_{N,TANK}(t_o) \quad (19)$$

145 where t_o and t_f represent the initial and final times, respectively, and the chlorine masses
 146 in pipes ($M_{N,PIPE}$) and tanks ($M_{N,TANK}$) are computed as follows:

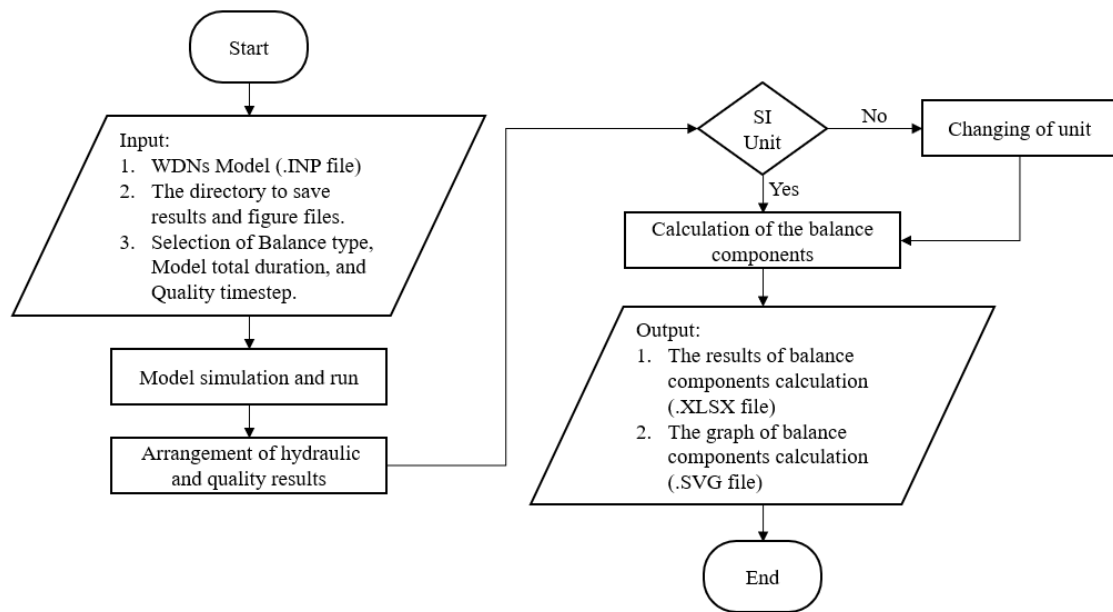
$$M_{N,PIPE}(t) = \sum_{i_{PIPE}=1}^{n_{PIPE}} C_{i_{PIPE}}(t) \forall_{i_{PIPE}} \quad (20)$$

$$M_{N,TANK}(t) = \sum_{i_{TANK}=1}^{n_{TANK}} C_{i_{TANK}}(t) \forall_{i_{TANK}}(t) \quad (21)$$

147

148 3. Software description

149 In this section, we describe the software requirements, input and output data, and
 150 GUI of KU2EPA-Balances. The package used for performing the hydraulic and water
 151 quality simulation in KU2EPA-Balances is the WNTR package in Python. Figure 4
 152 illustrates the flowchart to explain how our software works.



153

154 **Figure 4. Flowchart of KU2EPA-Balances**

- 155 • Software requirements

156 KU2EPA- Balances requirements include:

- 157 - A Python programming environment version 3.7
- 158 - WNTR version 0.2.2. installed in Python
- 159 - Users should be familiar with EPANET and Python programs.

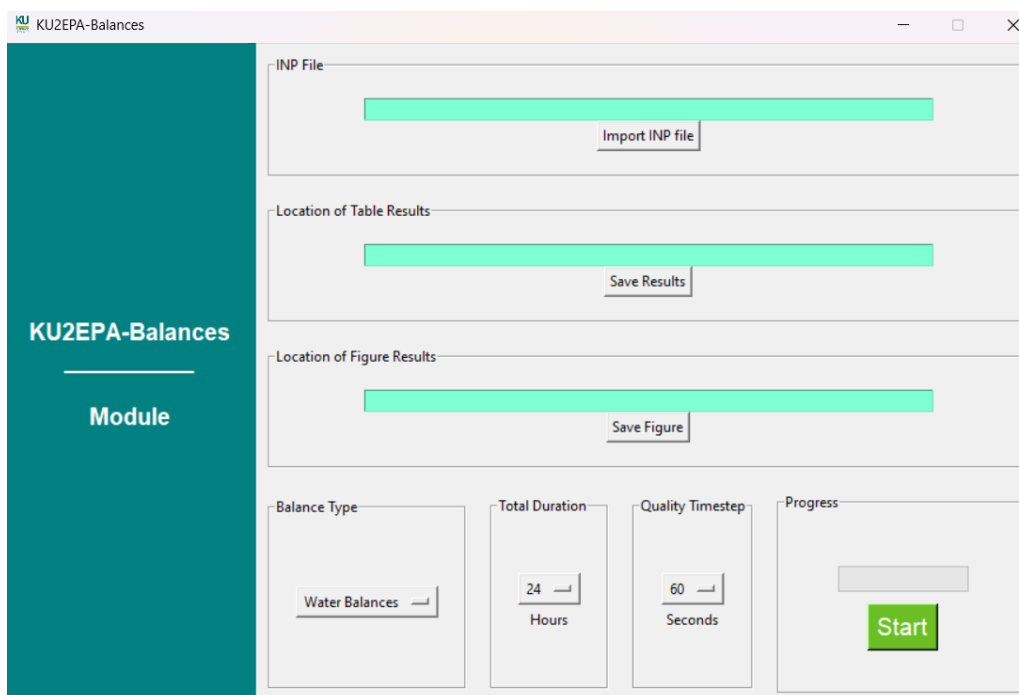
- 160 • Input data

161 The input data consists of the EPANET-based network model file in INP format,
 162 the chosen balance type, the total duration, and the quality time step. The INP file can be
 163 generated by exporting from EPANET or manually created in ASCII format identical to
 164 EPANET's INP file. The output data comprises hourly and daily balance tables, as well
 165 as main and detailed balance component graphs.

- 166 • Graphical User Interface (GUI)

167 Figure 5 shows the GUI of KU2EPA- Balances, designed to assist users and
 168 divided into seven sections:

- 169 - The "INP File" section allows users to import an INP network model file.
- 170 - The 'Location of Table Results' section allows users to select a folder and name
- 171 the table result file.
- 172 - The "Location of Figure Results" section allows users to select a folder and name
- 173 the figure result file.
- 174 - The "Balance Type" section allows users to select the balance type with three
- 175 options: Water balance, Energy balance, and Chlorine mass balance.
- 176 - The "Total Duration" section allows users to select the model's total duration in
- 177 hours.
- 178 - The "Quality Timestep" section is required when calculating the chlorine mass
- 179 balance type and allows users to select the water quality simulation timestep in
- 180 seconds.
- 181 - The "Progress" section allows users to start the computation and displays the
- 182 computation progress in percentages.



183 **Figure 5. KU2EPA-Balances graphical user interface**

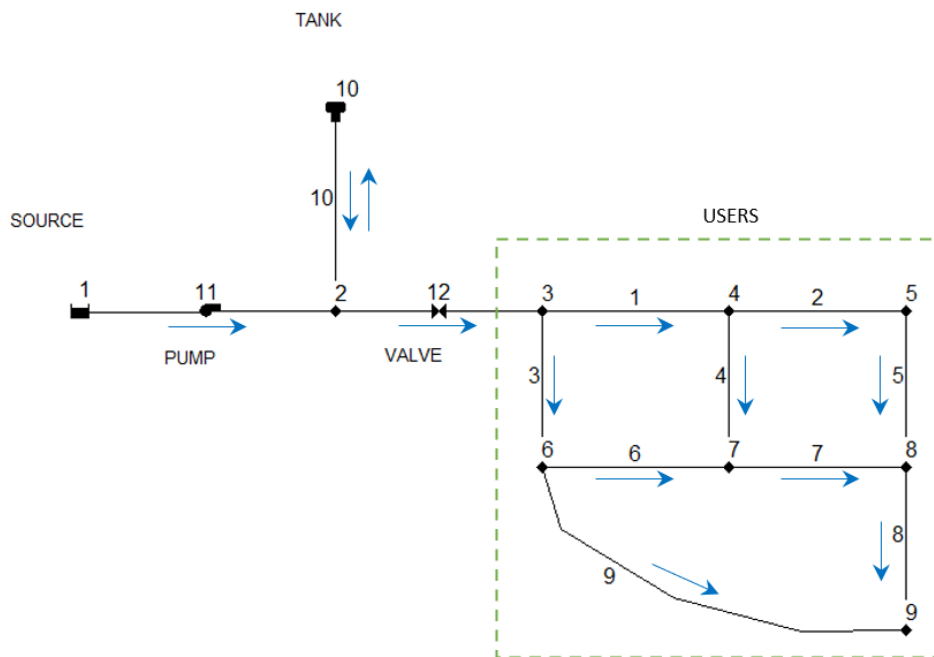
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185 4. Water distribution network example

186 Figure 6 displays a simplified WDN structure consisting of a reservoir, a pump, a
187 tank, junctions, pipes, and a valve. Potable water is pumped from the source (Node 1) to
188 the junction (Node 2). If the energy received from the pump (Link 11) surpasses the energy
189 in the tank (Node 10), the water will flow into the tank through the connected pipe (Link
190 10). Conversely, if the energy in the tank is higher, the water will flow out of the tank.
191 From the junction, water passes the valve (Link 12) into the service area, consisting of
192 pipes and junctions where users consume water. This example aims to demonstrate the
193 functionality of KU2EPA-Balances. Table 1 shows the properties of nodes and links. The
194 reservoir (Node 1) is characterized by a total head of -1 m and an initial quality of 1 mg/l.
195 The tank (Node 10)'s attributes include an elevation of 15 m, an initial water level of 5 m,
196 a minimum water level of 0 m, a maximum water level of 10 m, and a diameter of 3 m.
197 The pump (Link 11) has the performance with the designed flow of 70 m³/hr and the
198 designed head of 30 m. The valve (Link 12) in use is a pressure-reducing valve with a
199 control routine as follows:

- 200 - Setting pressure: 20 m at 12:00 AM.
- 201 - Valve open: 6:00 AM.
- 202 - Setting pressure: 25 m at 12:00 PM.

203 For leakage, the simulation employs the emitter function in (4) with an emitter
204 coefficient (c) of 0.2 and an emitter exponent (N_1) of 0.5 for all junctions. The initial
205 conditions can impact the results during the early stages of the simulation. Therefore, this
206 network example is simulated for a total duration of 96 hours with a quality timestep of 1
207 second. The results will be explained in the next section.



208
 209 **Figure 6. Water distribution network example, where arrows show flow**
 210 **directions, and service area is in dashed rectangle.**

211 **Table 1. Nodes and links properties**

Node	Base demand (m ³ /hr)	Link	Diameter (mm)	Length (m)	Roughness (H-W)
1	*	1	100	200	115
2	0	2	100	200	115
3	10	3	100	200	115
4	10	4	100	200	115
5	10	5	100	200	115
6	10	6	50	200	115
7	10	7	50	200	115
8	10	8	50	200	115
9	5	9	50	500	115
10	*	10	100	200	115
		11	*	*	*
		12	100	*	*

212 * Node 1 is a reservoir, Node 10 is a tank, Link 11 is a pump and Link 12 is a valve. The
 213 properties of these nodes and links are described in the context.

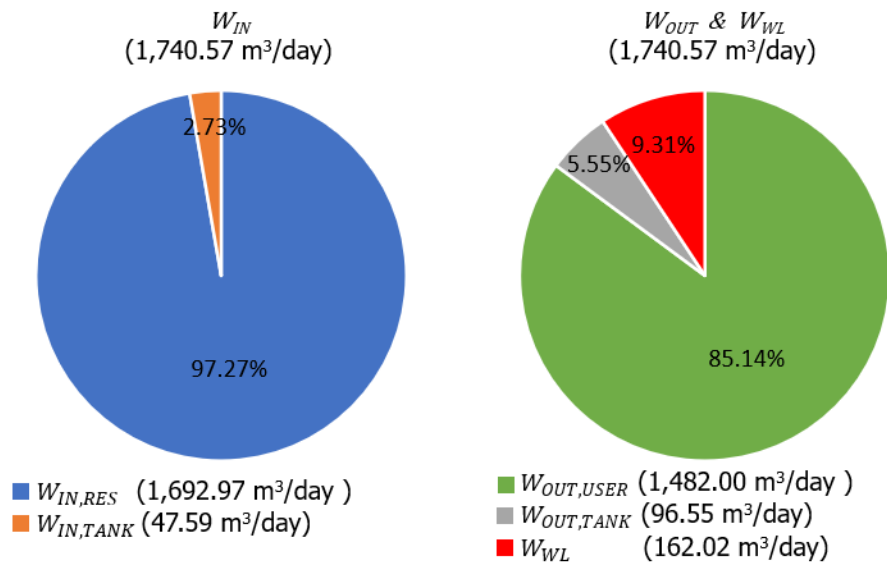
214 **5. Results and discussion**

- 215 • Water balance results

216 Figure 7 shows the simulation's water balance results. The daily water balance
 217 for Day 1, shown in Figure 7a, is indicated by two pie charts, inflow and outflow. From

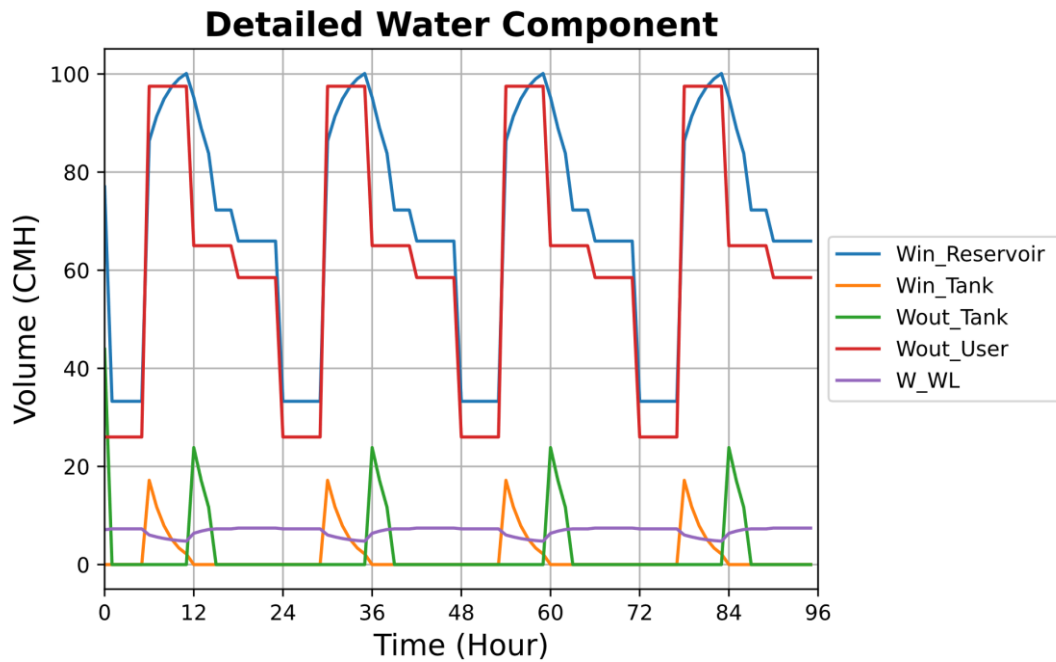
218 the inflow chart, the majority of the system input volume (W_{IN}) is sourced from the
 219 resource ($W_{IN,RES}$). From the outflow chart, most of the water exiting the system (W_{OUT})
 220 is delivered to users as $W_{OUT,USER}$. The water loss is 162.02 m³/day, accounting for 9.31%
 221 of W_{IN} . Additionally, the difference between $W_{IN,TANK}$ and $W_{OUT,TANK}$ reveals that a
 222 portion of W_{IN} (48.96 m³/day, calculated as 96.55 – 47.59) is used to fill the tank.

223 Figure 7b illustrates the hourly time series of water balance components ($W_{IN,RES}$,
 224 $W_{IN,TANK}$, $W_{OUT,TANK}$, $W_{OUT,USER}$ and W_{WL}) over 96 hours. Notably, the patterns of
 225 $W_{IN,RES}$ and $W_{OUT,USER}$ exhibit similarities. During the morning peak of water use, the
 226 system is partially supplied by the tank, leading to a sudden spike in $W_{IN,TANK}$.
 227 Subsequently, the tank is refilled, as indicated by a spike in $W_{OUT,TANK}$ immediately after
 228 the morning peak. The consistent value of W_{WL} over time indicates a constant rate of water
 229 loss due to the stable system pressure under the valve control.



230
 231

(a)



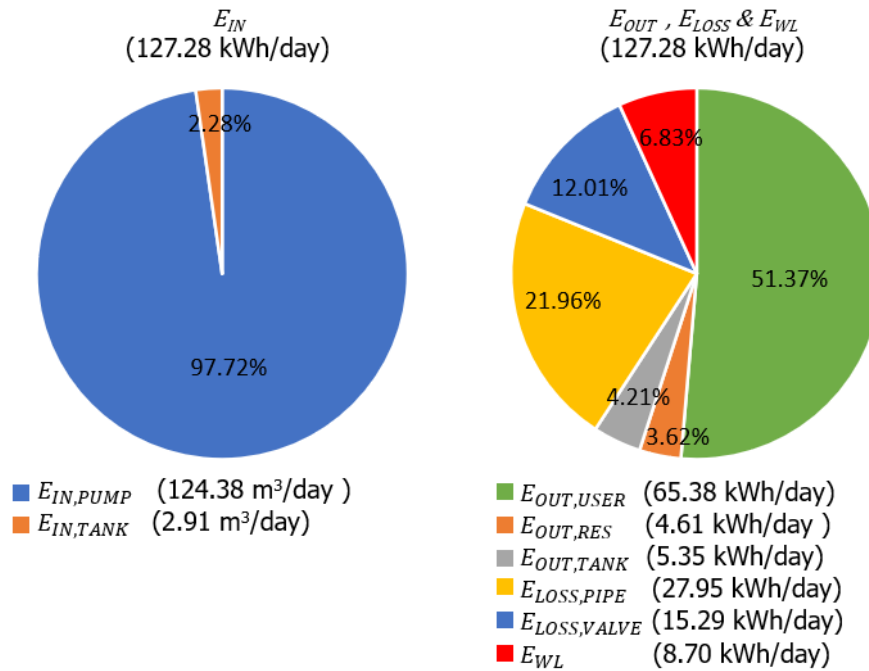
(b)

Figure 7. Water balance results with (a) daily balance for Day 1 and (b) hourly balance over 96 hours

- Energy balance results

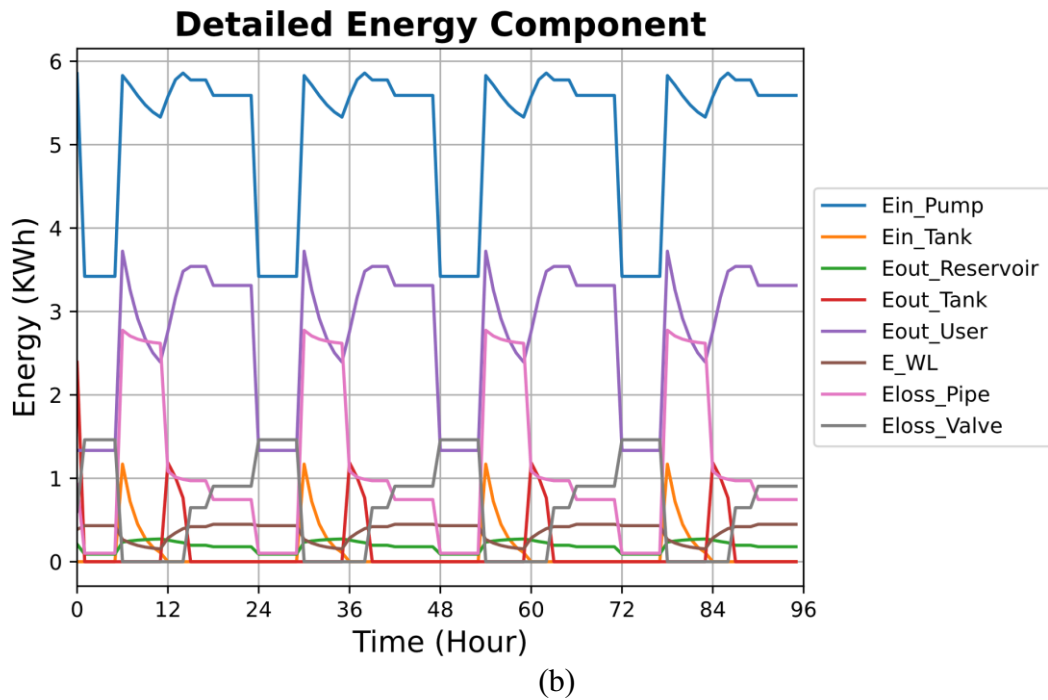
Figure 8 presents the simulation's energy balance results. The daily energy balance for Day 1 is illustrated into two pie charts as input and output energies in Figure 8a. The input energy chart reveals that the primary source of system input energy (E_{IN}) is the pump ($E_{IN,PUMP}$). While the water balance indicates that W_{OUT} is 90.69% of W_{IN} in Figure 7a, the energy outgoing through nodes (E_{OUT}) is only 59.20% of E_{IN} in the output energy chart. The discrepancy is attributed to the energy dissipated (E_{LOSS}), which accounts for 33.97% of E_{IN} . The difference between $E_{IN,TANK}$ and $E_{OUT,TANK}$ indicates that a portion of E_{IN} (2.44 kWh/day, calculated as 5.35 – 2.91) is stored in the tank, consistent with the tank's results in the water balance. In this particular example, $E_{IN,RES}$ is zero, while $E_{OUT,RES}$ is 4.61 kWh/day due to the negative total energy head of the reservoir.

248 Figure 8b illustrates the hourly time series of water balance components
 249 ($E_{IN,PUMP}$, $E_{IN,TANK}$, $E_{OUT,RES}$, $E_{OUT,TANK}$, $E_{OUT,USER}$, E_{WL} , $E_{LOSS,PIPE}$, and $E_{LOSS,VALVE}$
 250 over 96 hours. Notably, the patterns of $E_{IN,PUMP}$ and $E_{OUT,USER}$ exhibit similarities with a
 251 larger gap compared to the patterns of $W_{IN,RES}$ and $W_{OUT,USER}$ in the water balance due to
 252 energy dissipation. The pattern of E_{WL} over time is similar to W_{WL} , as both are influenced
 253 by system pressure. The morning peak of water use at 6:00 AM leads to a sudden increase
 254 in $E_{LOSS,PIPE}$, which gradually decreases until the next morning. $E_{LOSS,VALVE}$ is observed
 255 to depend on the valve control settings.



256
257

(a)



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259

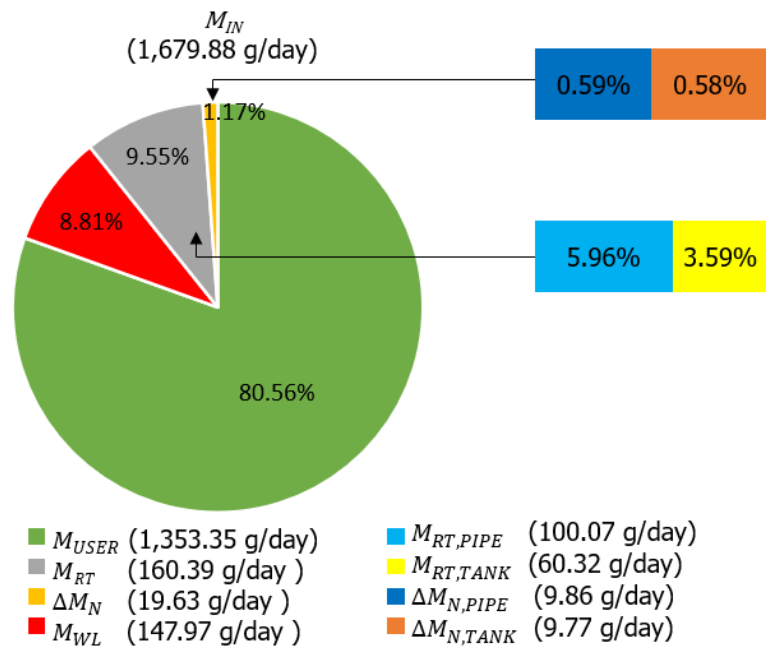
260 **Figure 8. Energy balance results with (a) daily balance for Day 1 and (b) hourly**
261 **balance over 96 hours**

262

- 263 • Chlorine mass balance results

264 Figure 9 shows the simulation's chlorine mass balance results. The daily chlorine
265 mass balance for Day 1, as presented in Figure 9a, reveals that the system input mass
266 (M_{IN}) is 1,679.88 g/day. Of this, a substantial portion, amounting to 1,353.35 g/day, is
267 delivered to users (M_{USER}), accounting for 80.56% of M_{IN} , while the outgoing mass
268 through water losses (M_{WL}) is 147.97 g/day, accounting for 8.81% of M_{IN} . Additionally,
269 the mass losses by reactions (M_{RT}) are 160.39 g/day, accounting for 9.55% of M_{IN} . The
270 chlorine mass changes (ΔM_N) amount to 19.63 g/day, which indicates the network requires
271 an additional mass input to achieve balance. This required mass is a result of the initial
272 conditions in this example, where there is no initial chlorine within the tank and pipes.
273 When the network continuously operates over a prolonged period with numerous cycles
274 of periodic patterns, ΔM_N will gradually approach zero.

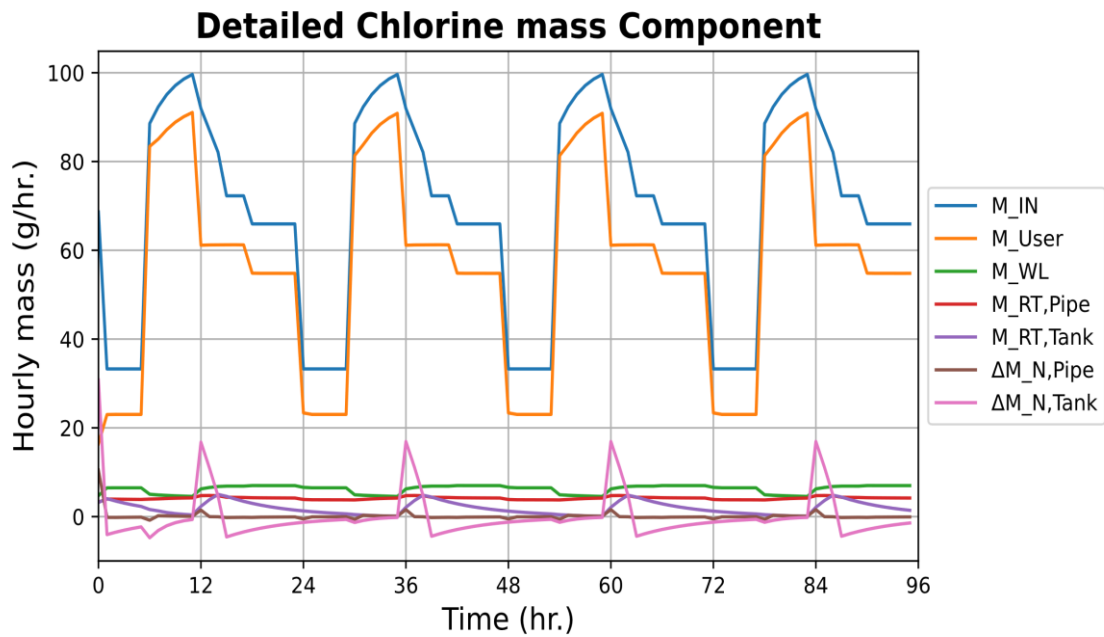
275 Figure 9b illustrates the hourly time series of chlorine mass balance components
 276 (M_{IN} , M_{USER} , M_{WL} , $M_{RT,PIPE}$, $M_{RT,TANK}$, $\Delta M_{N,PIPE}$, and $\Delta M_{N,TANK}$, over 96 hours.
 277 Notably, the patterns of M_{IN} and M_{USER} exhibit similarities. During the tank is refilled,
 278 chlorine is restored in the tank, leading to a sudden spike in $\Delta M_{N,TANK}$. Subsequently,
 279 $M_{RT,TANK}$ is increasing because of the decomposition of chlorine occurring inside the tank.



280

281

(a)



(b)

Figure 9. Chlorine mass balance results with (a) daily balance for Day 1 and (b) hourly balance over 96 hours

- Relationship between water losses, energy losses and chlorine losses

Mamade et al. (2018) first explored the relationship between water losses and energy losses. Analyzing simulation results from 20 real networks in Portuguese water distribution systems, they observed that the percentage of energy outgoing through water loss (E_{WL}) approximately equals to the percentage of water losses (W_{WL}). Later, Lipiwattanakarn et al. (2021a) conducted a theoretical energy balance analysis on simplified pipe networks and proposed a method indicating that the percentage of E_{WL} is actually smaller than the percentage of W_{WL} due to energy head loss. Our 1-day results show that the percentage of E_{WL} is 6.83% smaller than the W_{WL} percentage of 9.31%, agreeing with Lipiwattanakarn et al. (2021a)'s theory.

Recently, Wongpeerak et al. (2023) investigated the relationship between water losses and chlorine losses using a theoretical analysis similar to Lipiwattanakarn et al. (2021a). Their findings indicate that the percentage of outgoing mass through water losses

299 (M_{WL}) is also smaller than the percentage of W_{WL} . Our results confirm this theory, with
300 the percentage of M_{WL} at 8.81% being smaller than the W_{WL} percentage of 9.31%.

301 • Benefits of water, energy and chlorine mass balances

302 Using water balance and energy balance analyses, Lipiwattanakarn et al. (2019)
303 assessed the benefit of leak surveys and repairs of a water distribution network in the
304 service area of Metropolitan Waterworks Authority (MWA) in Bangkok, Thailand. By
305 comparing water and energy balances before and after the repairs, they observed a 9%
306 reduction of inflow volume to the network. Additionally, the input energy decreased by
307 8%, while the pressure and energy delivered to customers increased by 8%. To determine
308 the monetary benefit, they compared the cost of leak surveys and repairs with the benefits
309 gained from reduced water production and energy consumption. The study recommended
310 that MWA undertake more aggressive leak surveys and repairs based on these positive
311 outcomes. This example demonstrates the effectiveness of water, energy, and chlorine
312 mass balances in evaluating the benefits and losses of various activities or events. By
313 comparing the changes in each component of water, energy, and chlorine mass balances,
314 the benefits and losses can be assessed in terms of monetary value or service level. Our
315 KU2EPA-Balances software provides a convenient tool for researchers and practitioners
316 to analyze these balances effortlessly.

317 **6. Conclusion**

318 All potable water systems are dealing with water losses, energy losses and water
319 quality deterioration. These losses not only result in the wastage of water resources,
320 electrical energy, and chlorine but can also lead to the worsening or even disruption of
321 service to users. The balance concept is widely recognized and adopted to audit and
322 control these losses. Water distribution networks (WDNs) are typically the largest

323 components of potable water systems in terms of size and pipe length, making them the
324 most complex system to manage in terms of these losses.

325 However, there is currently no modelling tool available that can comprehensively
326 analyze and provide insights into these three critical aspects together. This paper
327 introduces KU2EPA-Balances, a new Python-based software designed to assist water
328 utilities in the calculations of water, energy, and chlorine mass balances and losses in
329 WDNs. KU2EPA-Balances utilizes WNTR, a Python package that integrates hydraulic
330 and water quality simulations. WNTR is built on the foundation of EPANET, the most
331 renowned software for simulating the movement and fate of potable water constituents in
332 pressurized distribution systems. The KU2EPA-Balances software has been applied to 20
333 real water distribution networks in the service area of Metropolitan Waterworks
334 Authority, Thailand (Lipiwattanakarn et al., 2021a; Wongpeerak et al., 2023) and verified
335 through manual calculations.

336 KU2EPA-Balances requires the EPANET input file, consisting of the pipe
337 network structure and properties such as pipes, pumps, tanks, reservoir, valves,
338 operational conditions, etc. The software demonstrates its capacity to accurately compute
339 water, energy, and chlorine mass balances even on short hourly timescales. In terms of
340 water balance, the software provides information on the volume of water loss
341 corresponding to system pressure. Regarding energy balance, it offers insights into energy
342 losses, including energies dissipated by pipes and valves, as well as energy outgoing the
343 system through leakage. In the context of chlorine mass balance, the software evaluates
344 chlorine mass losses due to the chemical reactions in pipes and tanks, as well as outgoing
345 chlorine mass through leakage. The information provided by KU2EPA-Balances can help

346 water utilities to plan suitable system operations, maintenance, and improvements to
347 achieve benefits in terms of water, energy and water quality in water distribution systems.

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